



## Test-field for evaluation of laboratory craters using a Crater Shape-based interpolation crater detection algorithm and comparison with Martian and Lunar impact craters

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### ABSTRACT

Impact craters are some of the most abundant geological features on most lunar and planetary bodies, providing insight into the history and physical processes that shaped their surface. It is therefore not surprising that extensive research has been done in the past on laboratory craters, as well as on crater detection algorithms (CDAs). No prior work has investigated how CDAs can assist in the research of laboratory craters, nor has an alternative formal method for evaluation of the similarity between laboratory and real impact craters been proposed. The result of this work is a test-field for evaluation of laboratory craters which includes: (1) a procedure for creation of explosion-induced laboratory craters in stone powder surfaces; (2) a method for 3D scanning of laboratory craters using a GOM-ATOS-I 3D scanner; (3) a new method for emplacement of laboratory craters into the topography of a planetary body; (4) a new method for objective evaluation of laboratory craters which utilizes the CDA, the Turing test, and a new measure of similarity between laboratory and real craters; and (5) a possibility of accompanying manual evaluation of laboratory craters using 2D topographical profiles. The successful verification of the proposed test-field, using Martian and Lunar global DEMs and local high-resolution DEMs, confirmed possibilities for the proposed scientific investigations of real impact craters using laboratory craters as proxies. This cost-effective approach also promises affordable accessibility for introductory physics and astronomy laboratories.

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### 1. Introduction

State-of-the-art image-analysis/object-recognition still does not offer an answer for how to design a crater detection algorithm (CDA) that is as robust as the scientific community would desire. This is a major motivation for several research groups that are working in this still young field, trying to achieve this goal. In general, CDAs are based on a large number of methods, including circle/ellipse detection (Cooper and Cowan, 2004; Flores-Méndez

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and Suarez-Cervantes, 2009; Krøgli and Dypvik, 2010), edge detections (Leroy et al., 2001; Sawabe et al., 2006) and alternatives to edge detections (Maass et al., 2011), Hough transform (Michael, 2003; Bue and Stepinski, 2007), conic section fitting and graph based edge organization (Kim et al., 2005), probability volume created by template matching (Bandeira et al., 2007), boosting (Martins et al., 2009), machine-learning (Stepinski and Urbach, 2008; Urbach and Stepinski, 2009; Stepinski et al., 2009; Ding et al., 2011; Liu et al., 2011), etc. The list of publications related to CDAs is constantly increasing (Cross, 1988; Taud and Parrot, 1992; Burl and Wetzler, 2011; Wang et al., 2011; Wan et al., 2012; Troglia et al., 2012; Bandeira et al., 2012).

The scientific research on laboratory craters has lasted even longer, with the main objective to model physical processes of creation of real impact craters. A major motivation for laboratory studies of impact craters is the relatively small number of terrestrial craters (Grieve, 1987; French, 1998), and the inaccessibility of extraterrestrial impact

craters. Fechtig et al. (1972) described techniques for accelerating  $\mu\text{g}$ -,  $\text{mg}$ - and  $\text{g}$ -sized particles to meteoroid velocities (up to 50 km/s), used in order to study Lunar craters. Schmidt and Holsapple (1980) used Boeing 600-G geotechnic centrifuge in order to study, among others, the influence of gravity on cratering. Laboratory craters have additionally been used for studying: impact spallation experiments (Polansky and Ahrens, 1990); relationships between impact and ejection velocities (Cintala et al., 1998); depth of cracking beneath impact craters (Ahrens et al., 2001); hypervelocity impact cratering in ice (Burchell et al., 2001; Grey et al., 2001); crater formation on ice silicate mixture targets (Hiraoka et al., 2007); the differences between the results of impacts on  $\text{CO}_2$  targets with those on  $\text{H}_2\text{O}$  ice targets (Burchell et al., 2005); marine impact events (Ormö, 2005; Milner et al., 2008); cratering in layered surfaces (Senft and Stewart, 2007); effects of target properties (Barnouin-Jha et al., 2007); ejecta emplacement of Martian craters (Suzuki et al., 2007); crater excavation and formation of an uprange forbidden zone in an oblique impact (Herrick et al., 2008); ejecta fragmentation in impacts into gypsum and water ice (Miljković et al., 2011), etc. How to apply laws obtained using laboratory craters to real impact craters is certainly one of the most challenging issues. Hence, a possibility of using laboratory craters as a proxy to real ones has also been intensively studied (Desai et al., 2007, 2008; Ransom, 2011). One of the results is that even at  $\mu\text{m}$  scale it is possible to create simple and complex craters in laboratories (Desai et al., 2010). It is expected that different approaches to numerical modeling of impact events will contribute to these issues in future (Collins et al., 2005; Davison et al., 2011).

No previous work has investigated whether it is possible to use CDAs for the evaluation of laboratory craters. Additionally, all previous evaluations of laboratory craters have been done manually, which certainly has a disadvantage—subjectivity of the approach. This was a motivation for our investigation of the possibility of using CDAs for evaluation of laboratory craters. The preliminary results have been recently presented (Vojković et al., 2010a, 2010b; Salamunićar et al., 2010; Vinković et al., 2011), while the completed results are given in this paper. In order to provide reproducibility of the methods presented in this paper, 3D scans of our laboratory craters and the source code (Craters5\_81.zip) of the interpolation-based CDA used in this paper have been made available online (Salamunićar and Lončarić, 2011). In Section 2 we present methods and datasets of this paper in detail. The results of our study are presented in Section 3 and the conclusion is given in Section 4.

## 2. Methods and datasets

### 2.1. Creation of explosion-induced laboratory craters in stone powder surfaces

The experiments were performed on fine dry stone powder surfaces of a material with negligible strength, produced in a local

limestone quarry as a by-product of stone cutting. The usage of stone powder instead of hard rock targets gives a possibility to simulate large-scale events with small amounts of explosive charges, as explained in Section 3.1. The powder was placed in containers much larger than the finally obtained craters. The powder was compressed so that the surface density was  $1.5\text{--}1.9\text{ g/cm}^3$ , as shown in Table 1. In our case, the silver acetylide ( $\text{Ag}_2\text{C}_2$ ) explosive charge was used for crater formation. Cylindrically shaped charges were buried just below the surface. The charge mass was  $105\text{--}350\text{ mg}$  and the cylinder height/width was  $0.375\text{--}1.5$ , as shown in Table 1. Explosive charges were ignited using a laser. We used silver acetylide for explosive charges because it is easily accessible in small quantities as a by-product of regular chemistry classes. One of our objectives was similar to the work by Kasas et al. (2000) and Claycomb (2009)—the creation and study of craters to be affordable to low-budget laboratories, and with this to a large number of students.

### 2.2. Scanning of laboratory craters using a 3D scanner

Laboratory craters were scanned in 3D to produce a high-accuracy digital topography of their shape. The device GOM-ATOS-I used for digitizing the craters is based on the principle of stereo-photogrammetry, which projects structured light patterns onto the surface of the object and captures the image using two CCD cameras, each with a resolution of  $1032 \times 776$  pixels. Different line patterns are projected onto the surface in a time sequence to enable simple identification of the spatial positions of measurement points. Based on the stereo scans of the deformed projected lines and using triangulation, the 3D-shape of the surface is determined accordingly. More detailed description of the GOM-ATOS-I device is available online (GOM, 2012).

### 2.3. Turing test and measure of similarity between laboratory and real craters

The objective is to provide a formal method for measuring the similarity between laboratory and real craters. We developed an approach based on CDAs and 3D-shapes of laboratory craters which utilizes the Turing test (Saygin et al., 2000): if a laboratory crater is sufficiently similar to the real one to be detected via the CDA then we consider this to be a satisfactory model, otherwise it is rejected as insufficiently similar. In order to perform a more advanced measurement of similarity, an A-ROC (also referenced in the literature as a ROC' curve) evaluation of CDAs can be used. Each position of a laboratory crater on the A-ROC curve corresponds to a probability threshold, which defines the working mode of CDA wherein only those detections with higher assigned probability than the threshold are accepted. During detection of a laboratory crater, the CDA assigns to it a probability that it is an impact crater in the same way as for detections of real craters.

**Table 1**  
Basic information on our laboratory craters (\*explosive charge cylinder diameter is 8 mm).

Craters	Attributes				
	Surface density of used material [ $\text{g/cm}^3$ ]	Explosive charge cylinder depth* [mm]	Explosive charge cylinder mass [mg]	Depth of resulting crater [mm]	Diameter of resulting crater [mm]
lab-crater-1	1.90	8	$197 \pm 10$	15.8	49.5
lab-crater-2	1.80	11	$295 \pm 10$	12.9	45.2
lab-crater-3	1.70	8	$190 \pm 10$	13.1	43.8
lab-crater-4	1.80	3	$105 \pm 10$	5.9	29.7
lab-crater-5	1.57	5	$165 \pm 10$	9.5	39.2
lab-crater-6	1.75	5	$179 \pm 10$	10.7	41.8
lab-crater-7	1.75	12	$350 \pm 10$	21.7	61.3

This defines its position on the A-ROC curve, where the probability assigned to a laboratory crater is equal to the probability threshold. When a crater is closer to the bottom-left corner of the A-ROC curve, it is detected with larger associated probability that it is indeed a crater, and therefore its 3D-shape is more similar to real craters. In our case, as a measure we use a percentage of the distance from the top-right corner to the position of a laboratory

crater on the A-ROC curve, as defined with Eq. (1) (for definitions of TDR and FDR see Table 2). If, on the contrary, a similarity between laboratory crater and some particular real crater is required, a percentage of the distance between the position of a laboratory crater on the A-ROC curve and the position of a real crater on the A-ROC curve can be used:

$$p_{lc} = \sqrt{\frac{(1-TDR)^2 + (1-FDR)^2}{2}} \quad (1)$$

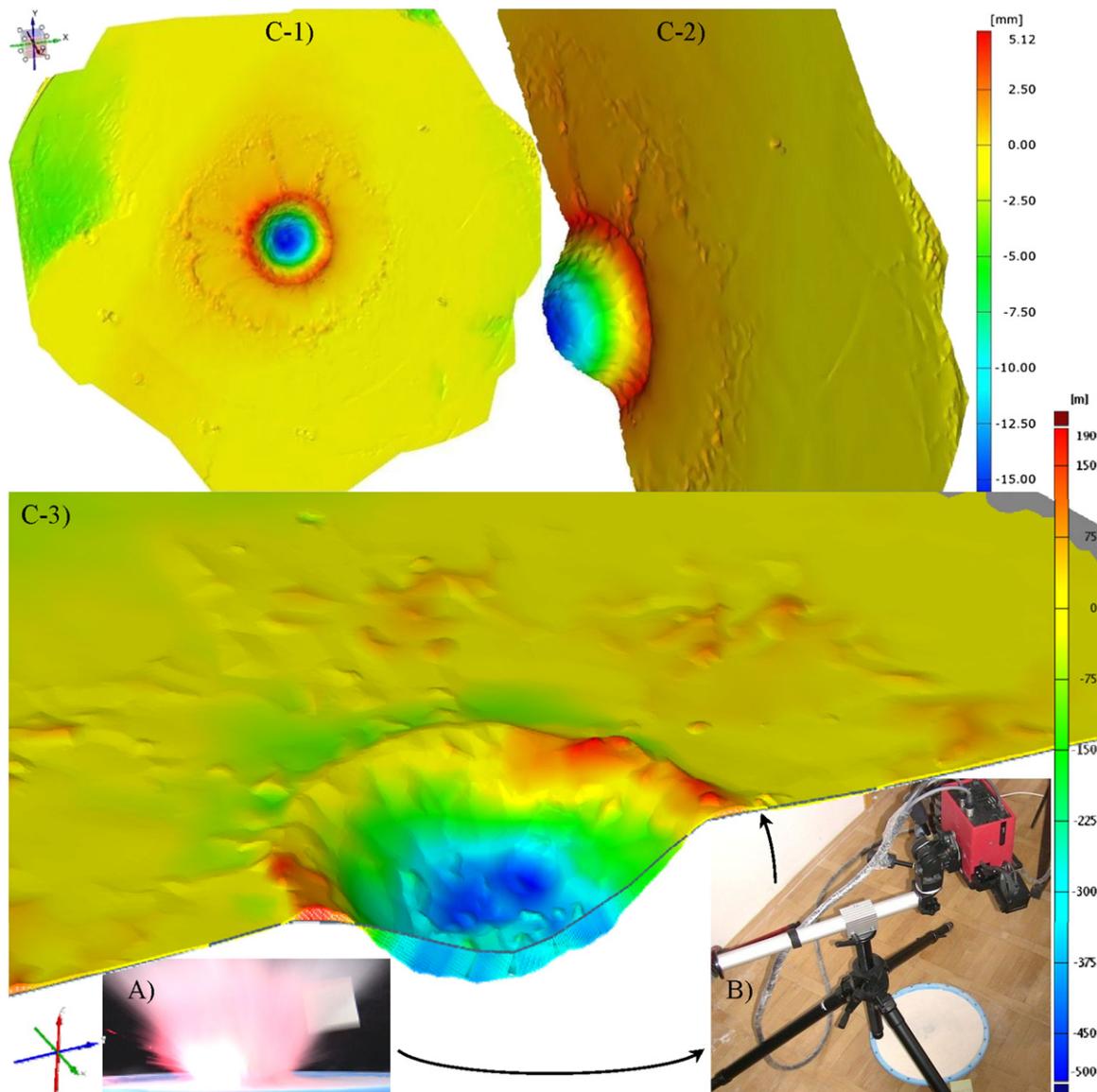
**Table 2**

Definitions and graphs (TP=true positives; FP=false positives; FN=false negatives; GT=ground truth; TDR=true detection rate; FDR=false detection rate; ROC=receiver operating characteristics; F-ROC=free-response ROC; A-ROC=approximation of ROC) used for evaluation of CDAs (Salamunićar et al., 2012).

Used definitions	Used graphs [horizontal range/vertical range]
GT=TP+FN TDR=TP/(TP+FN)=TP/GT FDR=FP/(TP+FP)	F-ROC [TP/FP] A-ROC [TDR/FDR]

#### 2.4. Emplacement of laboratory craters in the topography of a planetary body

In order to perform the Turing test, including measurement of similarities between laboratory and real craters, 3D-scans of laboratory craters need to be emplaced in the topography of a planetary body. The objective for emplacement is to provide a smooth transition between the surrounding topography and a laboratory crater, and at the same time to preserve the topography of the laboratory crater. The four major steps of the method are as follows:

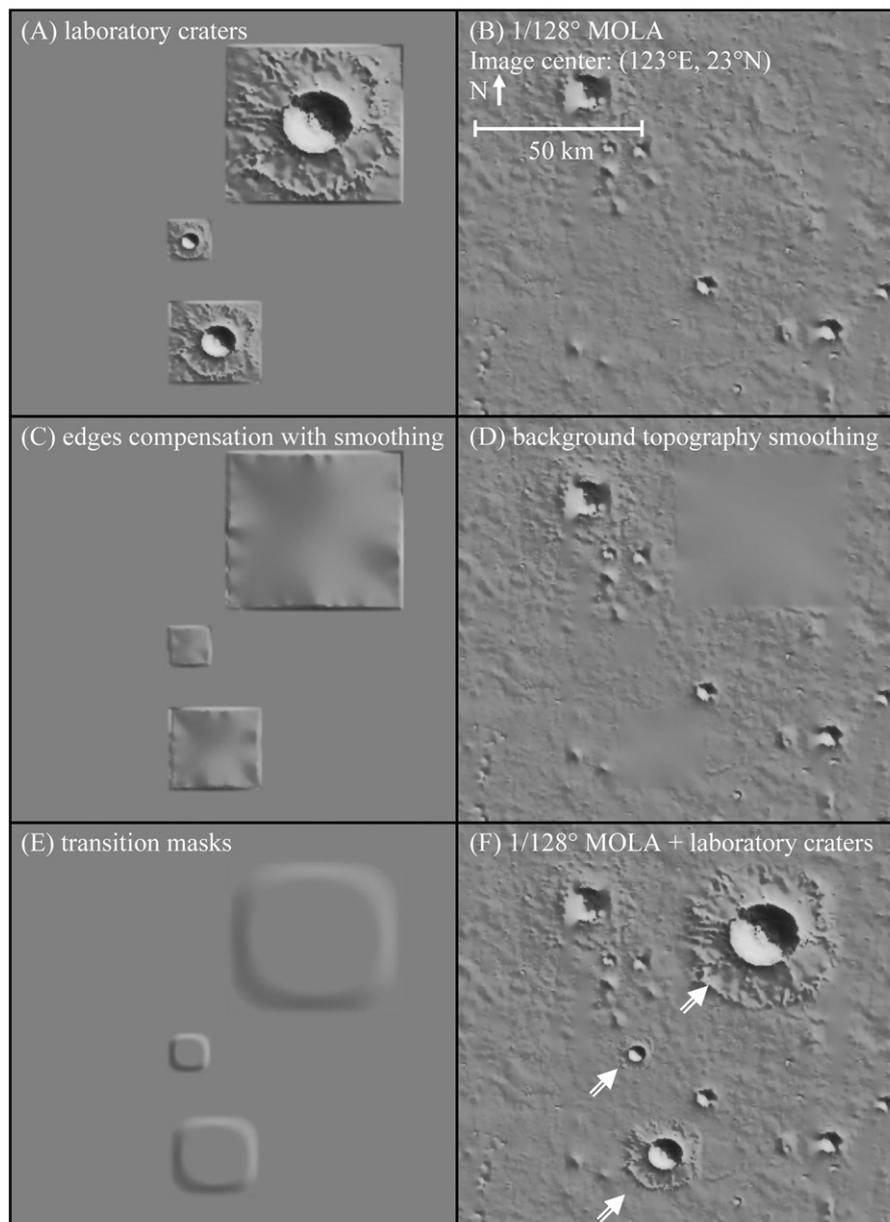


**Fig. 1.** Scanning of an explosion-induced laboratory crater (A) using a 3D scanner (B), resulting profiles (C-1 and C-2), and comparison of our laboratory crater and Martian crater S027098B13104K01753T56623Y2007S ( $D=5.1$  km) from MA132843GT catalog rendered using 1/128° MOLA data (C-3).

(1) identification of rectangles associated with the coordinates (top, bottom, left, and right) of each individual laboratory crater (in the following text: object-rectangle); (2) compensation for values close to the rectangle's edges with smoothing (in the following text: correction-1); (3) smoothing of places where laboratory craters will be emplaced (in the following text: correction-2); and (4) creation of a transition mask between the laboratory crater and the background topography (in the following text: transition-mask). The summary of the method is as follows: (1) it takes values from a laboratory crater's 3D-scan; (2) they are decreased with correction-1 values; (3) they are increased with correction-2 values; (4) the transition-mask's values are used for interpolation between the values computed in the previous step and the values of background topography. The objective of correction-1 is to prevent sharp transition between the background topography and an emplaced laboratory crater. The objective of correction-2 is to prevent superposition of the geological features from the background topography to the shape of the

laboratory crater. The objective of the transition-mask is to provide a smooth transition between surrounding topography and the laboratory crater.

Each object-rectangle is defined as the smallest rectangle, with the first and last row and column containing at least one value different from 0. The algorithm for correction-1 and correction-2 is as follows. In the first step, correction values are defined, such that the distance to object-rectangle is 1, 2 or 3 pixels, as an average value for masks sized  $3 \times 3$ ,  $5 \times 5$  and  $7 \times 7$  pixels, respectively. In the second step the remaining correction values are defined, using values at the distance of 3 pixels from the object-rectangle. They are averaged using a weight factor that is inversely proportional to  $d^4$ , where  $d$  is the distance in pixels from the pixel of interest to the used correction value. The algorithm for the transition-mask is as follows. Within each object-rectangle two rectangles are defined with rounded corners. For values outside the larger of these, background topography values will



**Fig. 2.** Steps of laboratory crater emplacement: (A) 3D-scans of laboratory craters; (B) background topography; (C) compensation of values close to edges with smoothing; (D) smoothing of places where laboratory craters will be emplaced; (E) transition masks between laboratory craters and background topography; and (F) emplaced laboratory craters.

be used as final without modification. For values inside the smaller, processed values of the laboratory crater's 3D-scan will be used as final without modification. For values between the two rectangles with rounded corners, linear interpolation is used to provide transition between two digital elevation maps (DEMs).

### 2.5. Crater detection algorithms and extraction of topographical profiles of laboratory craters

In our previous work, we developed a CDA for crater detection from digital topography data using gradient value/orientation, morphometry, votes-analysis, slip-tuning and calibration (Salamunićcar and Lončarić, 2010; in the following text: CDA<sub>1</sub>) and further improved it using a Crater Shape-based interpolation (Salamunićcar et al., 2012; in the following text: CDA<sub>2</sub>). Both versions use: (1) multi-resolution image analysis; (2) various edge-detection methods, with the best results provided by Canny (in the following text: CDA<sub>1</sub>-Canny and CDA<sub>2</sub>-Canny) and by Shen-Castan (in the following text: CDA<sub>1</sub>-Shen-Castan and CDA<sub>2</sub>-Shen-Castan); and (3) the Hough transform (also referenced in the literature as a Radom-Hough transform). Once the 3D-shape of a laboratory crater is emplaced in e.g. Martian or Lunar topography, the CDA can also be used to extract profiles of laboratory craters in the same way as for real craters. Such an approach ensures that profiles of real and laboratory craters are extracted in the same way, and with this prepared for further analysis.

### 2.6. Datasets used for test-fields

We used datasets prepared in our previous work (Salamunićcar et al., 2012) based on Mars orbiter laser altimeter (MOLA) dataset

(Smith et al., 2003) and Lunar orbiter laser altimeter (LOLA) dataset (Smith et al., 2010). Additionally, we used some high-resolution Martian and Lunar DEMs.

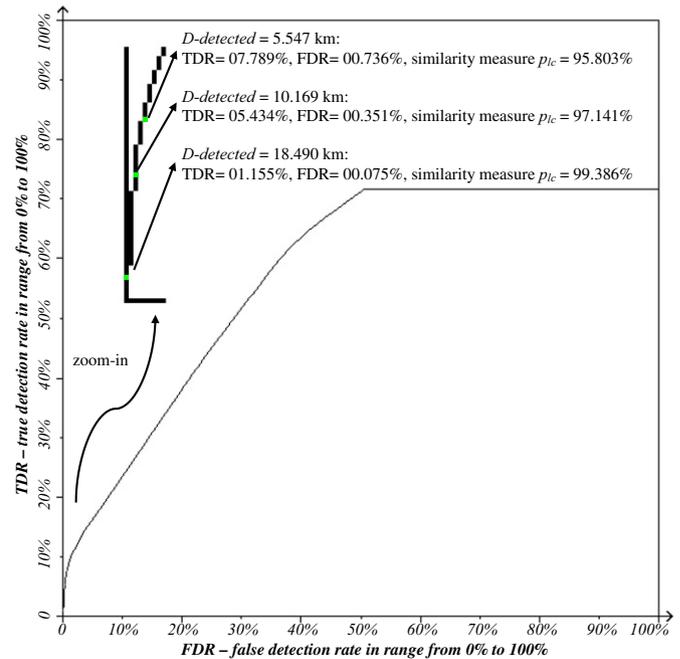


Fig. 4. An example of the estimation of the similarity between laboratory and real impact craters using Eq. (1) and the A-ROC evaluation of CDAs based on true and false detection rates.

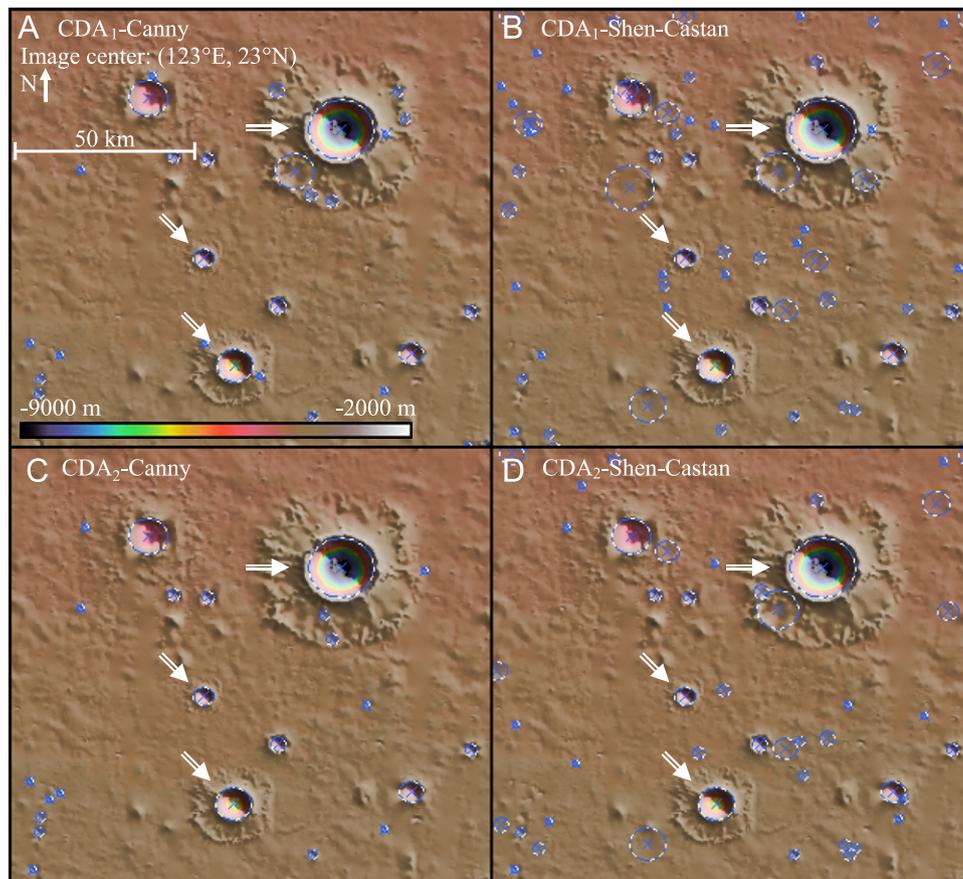


Fig. 3. Detections of laboratory craters in the context of the real topography using: (A) CDA<sub>1</sub>-Canny; (B) CDA<sub>1</sub>-Shen-Castan; (C) CDA<sub>2</sub>-Canny; and (D) CDA<sub>2</sub>-Shen-Castan.

### 3. Results and discussion

#### 3.1. Basic properties of laboratory craters created

Craters on planetary and lunar surfaces display a simple–complex transition from the smaller, mostly very circular bowl-shaped craters, to larger complex craters with central peaks, and to the largest multi-ring impact basins (Melosh and Ivanov, 1999). The theory of simple impact craters distinguishes between the strength regime and the gravity regime of cratering (Holsapple, 1993, 1994). The strength regime is applied when the strength of a soil surface is large compared to the gravitational pressures within the ground surface at depths comparable to the impactor size. Under such conditions the crater shape is dictated by the soil properties. The gravity regime is applicable when the soil strength is much smaller than the gravity pressure. Under that regime the crater shape is dictated by the impactor's size and velocity for a given planet surface gravity. It is exactly the gravity regime that we encounter in the case of asteroidal impactors, where kinetic energy is large enough to ignore the soil strength. At the instant of impact, large volumes of target rock are shattered, deformed, melted, and even vaporized in a few seconds (French, 1998). An object only a few meters across ( $\sim 6$  m) carries the kinetic energy of an atomic bomb (Hiroshima, Japan  $\sim 20$  kT of TNT equivalent) and results in a considerably larger crater ( $D=120$  m) while the energy release in an impact event is virtually instantaneous (French, 1998). The immediate energy release can be treated with the classical physics of point source explosions where the actual source of energy is irrelevant. This approach has been used to successfully explain the morphology of impact craters (Holsapple, 1993). Alternatively, we can enable the gravity regime if the soil strength is close to zero, such as in our stone powder material, while the point source explosion is induced by an explosive charge of lower yield than actual asteroid impacts. The results show that our experimental cratering can be used as a proxy for simple Martian and Lunar craters formed under the gravity regime, even though depths of our laboratory craters are 5.9–21.7 mm and diameters are 29.7–61.3 mm, as shown in Table 1.

#### 3.2. Resulting 3D-scans of laboratory craters created

An example of a 3D-scan of an explosion-induced laboratory crater is shown in Fig. 1. A comparison with a similar profile of a Martian crater with a high depth/diameter ratio is also shown. As can be seen, the 3D-scans are highly accurate representations of craters' shapes. In addition, the scans show that our laboratory craters contain a well formed crater rim, as well as crater ejecta blanket at a distance between rim and approximately two craters' radii. Accordingly, at least the most important morphological properties of simple craters can be modeled in a laboratory and accurately digitalized for further analysis and comparison with real impact craters.

#### 3.3. Results of laboratory craters' emplacement for three different sizes

The method for emplacement of a laboratory crater's 3D-scan works satisfactorily, as shown in Fig. 2. The transition between surrounding topography and laboratory craters is smooth, while at the same time the topography of the laboratory crater is preserved. For the purpose of method illustration, some intermediate steps are shown as well: correction-1's values in frame (C); correction-2's values in frame (D); and the transition-mask's values in frame (E). The method works successfully for different sizes, as shown in frame (F).

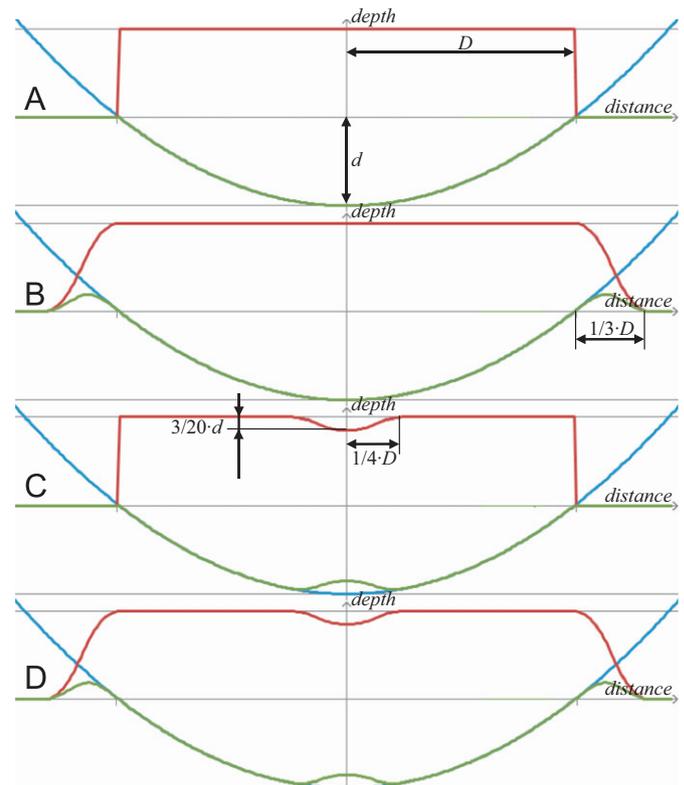
#### 3.4. Results for different crater detection algorithms and accompanying evaluation

CDA<sub>2</sub> provides better results than CDA<sub>1</sub>. In addition, results are better for Canny based CDAs than for those based on Shen-Castan. However, in this work we are using all four versions (CDA<sub>1</sub>–Canny, CDA<sub>1</sub>–Shen-Castan, CDA<sub>2</sub>–Canny and CDA<sub>2</sub>–Shen-Castan), because this is the best possible test of the overall robustness of the approach that can be currently performed. As shown in Fig. 3, detections via different CDAs are similar but still different.

An example of the estimation of similarity between laboratory and real impact craters using Eq. (1) and the A-ROC evaluation of CDAs is shown in Fig. 4. The same laboratory crater is scaled to three different sizes in order to test how this influences overall results. The largest one is detected via the CDA with the largest associated probability because, for larger craters, the associated large depth/diameter ratio is a stronger indication that the detected object is a crater. However, differences between these three cases are not great, as expected, because the same laboratory crater is emplaced in three different sizes.

#### 3.5. Martian and Lunar based test-fields and resulting profiles of laboratory craters

Mathematical modeling of impact craters using parabola segments is shown in Fig. 5. With such an approach, it is possible to model simple impact craters with rim, central peak, or both. Martian and Lunar test-fields for laboratory craters are shown in



**Fig. 5.** Mathematical modeling of impact craters using parabola segments (functions of form  $y=ax^2+bx+c$ , where  $x$  is distance and  $y$  is depth), the model of an impact crater (green) is the product of basic parabola (blue) and modification function (red) which goes vertically between 0 and 1: (A) an impact crater without rim and without central peak; (B) an impact crater with rim but without central peak; (C) an impact crater with central peak but without rim; and (D) an impact crater with rim and with central peak. (For interpretation of the references to color in this figure legend, the reader is referred to the web version of this article.)

Fig. 6. In addition to laboratory craters and mathematical models, cross, triangle, quadrangle and hexagon artificial objects are used in order to test the overall approach. The basic idea is as follows: for shapes more similar to real craters, the measure of similarity should provide larger values. In principle, the results including profiles for Martian topography are similar to the results for Lunar topography, as expected. There are some smaller differences, but this is also expected for different parts of the topography of the same lunar or planetary body. In our case, we selected parts of the global topography, which is mostly flat, in order that shapes could be embedded in it without considerable distortions. Selected

parts also contain some roughness, in order to evaluate how this influences the results.

### 3.6. Cross-comparison of detection results

Detections of  $CDA_2$ -Canny for the Martian test-field are shown in Fig. 7 and for the Lunar test-field in Fig. 8. The artificial object cross is not detected in either size or test-field. The artificial objects triangle and quadrangle are detected in only some cases. The artificial object hexagon is detected in all sizes and both test-fields. According to the Turing test, the cross is insufficiently

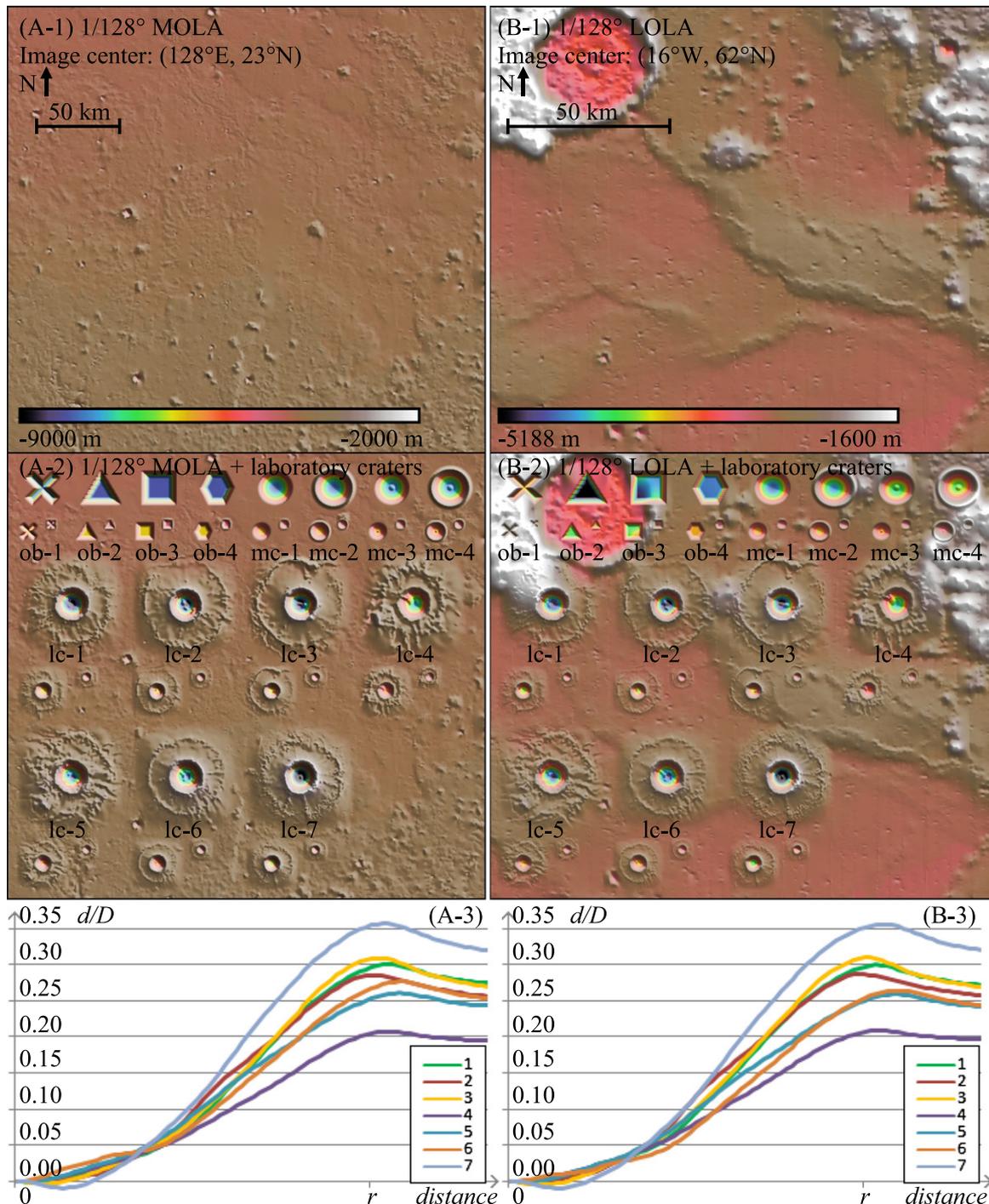
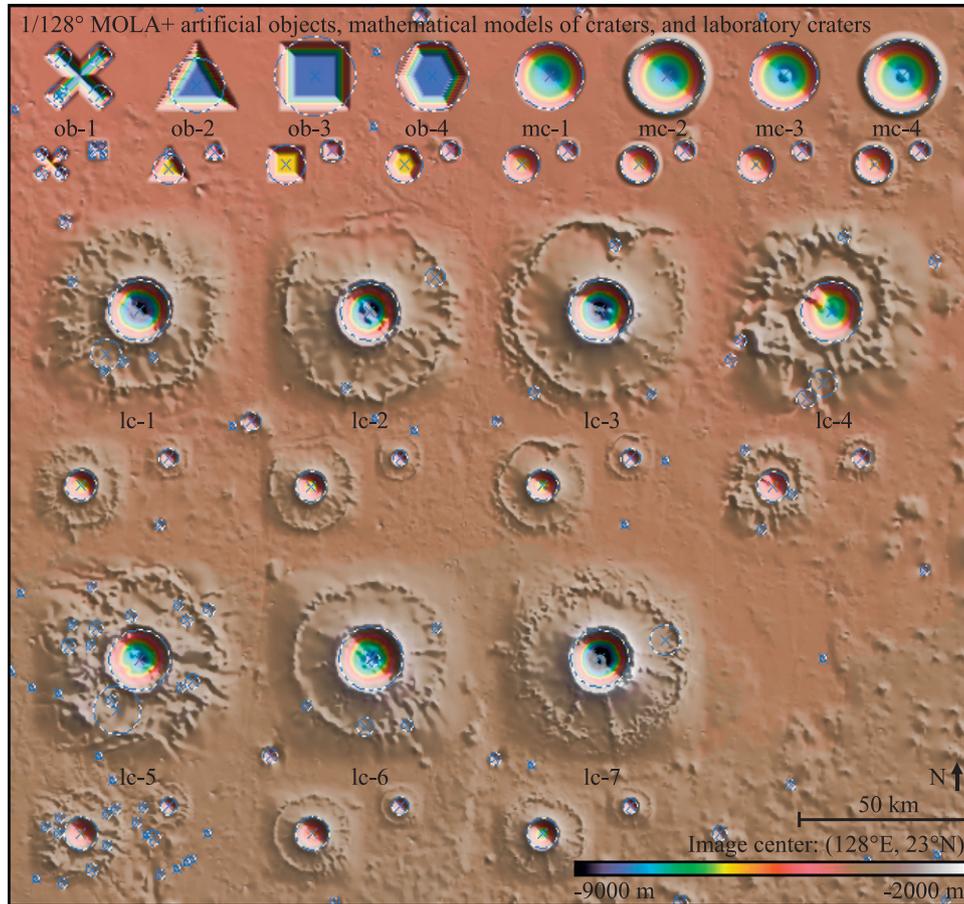
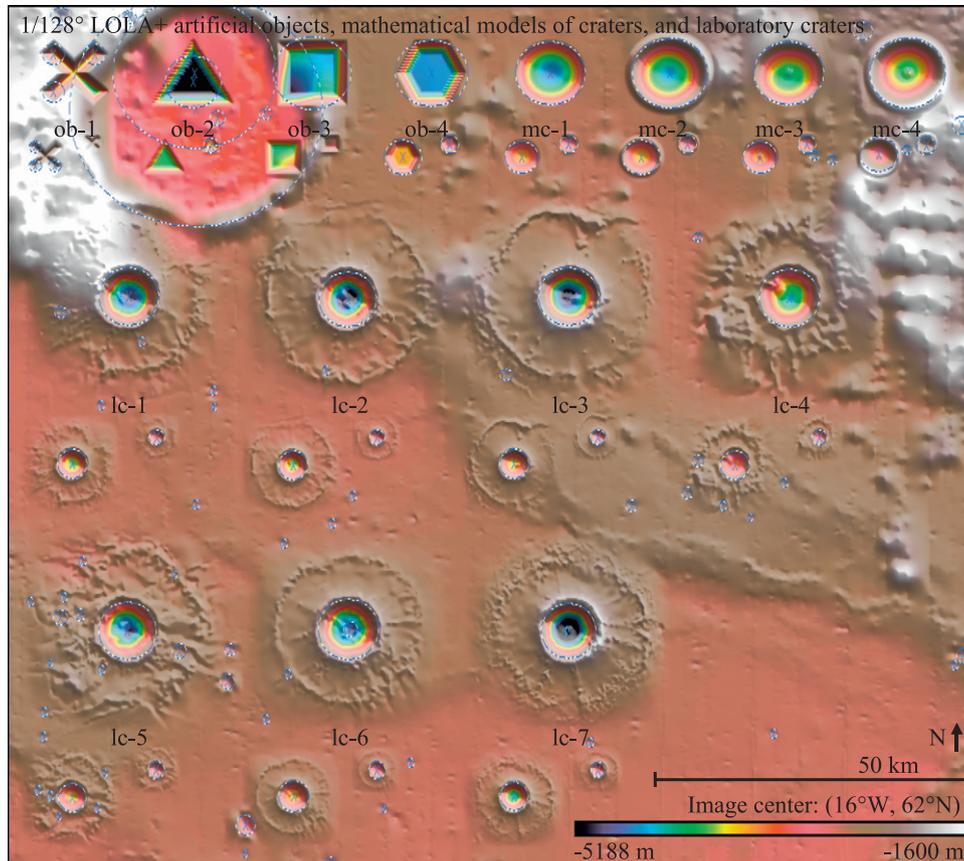


Fig. 6. Martian (A-\*) and Lunar (B-\*) test-field for cross, triangle, quadrangle and hexagon artificial objects (ob-\*), mathematical models of craters (mc-\*), and laboratory craters (lc-\*): initial topography (top row), embedded diverse shapes (middle row), and profiles of laboratory craters (bottom row).



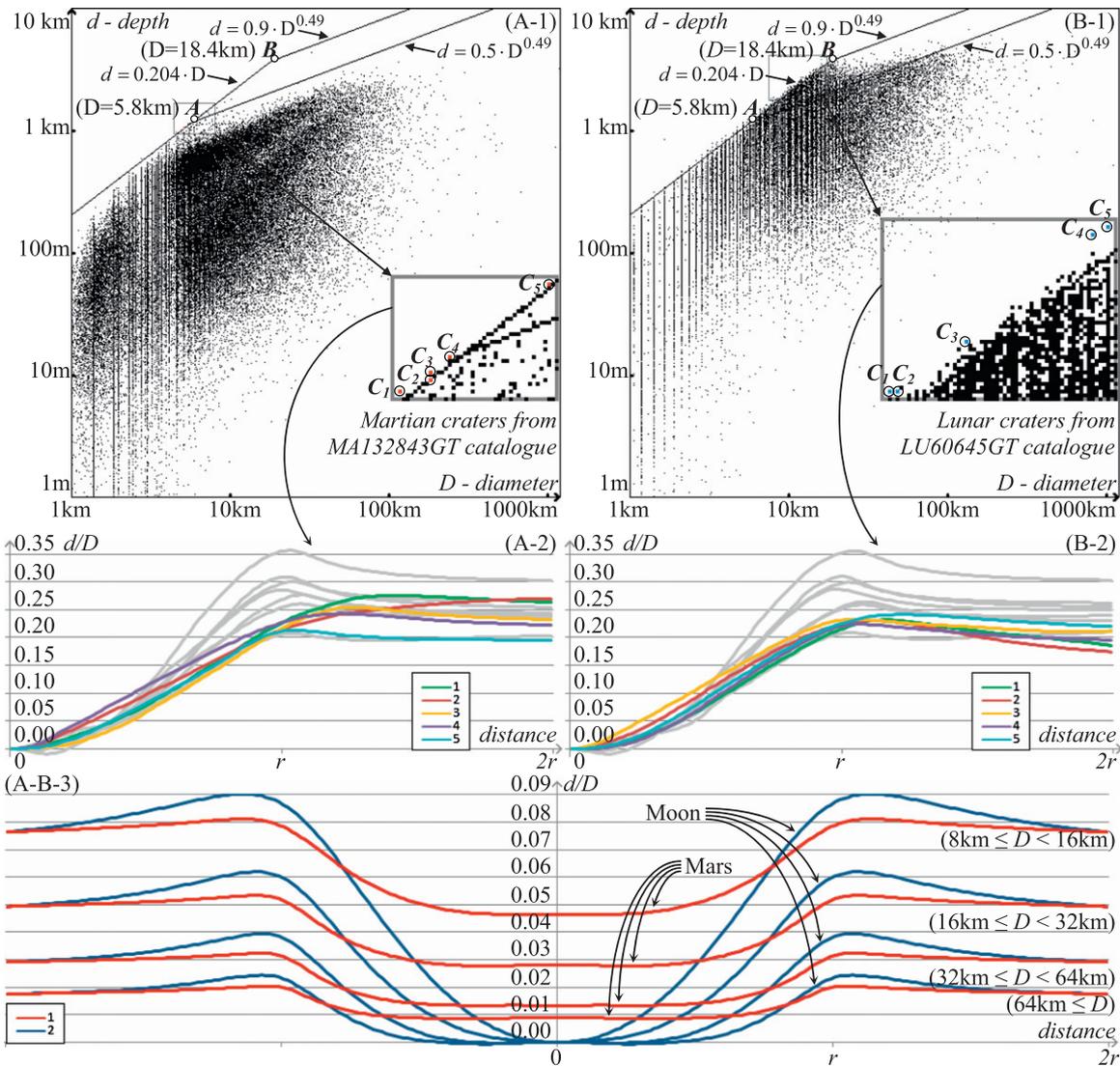
**Fig. 7.** Detections of cross, triangle, quadrangle and hexagon artificial objects (ob-\*), mathematical models of craters (mc-\*), and laboratory craters (lc-\*), embedded in Martian topography, using CDA<sub>2</sub>-Canny.



**Fig. 8.** Detections of cross, triangle, quadrangle and hexagon artificial objects (ob-\*), mathematical models of craters (mc-\*), and laboratory craters (lc-\*), embedded in Lunar topography, using CDA<sub>2</sub>-Canny.

**Table 3**  
Results of the evaluation of artificial objects (cross, triangle, quadrangle, hexagon), mathematical models of craters (math-crater-\*), and laboratory craters (lab-crater-\*), for the largest size, using diverse CDA-s and topographies (X means that the Turing test failed).

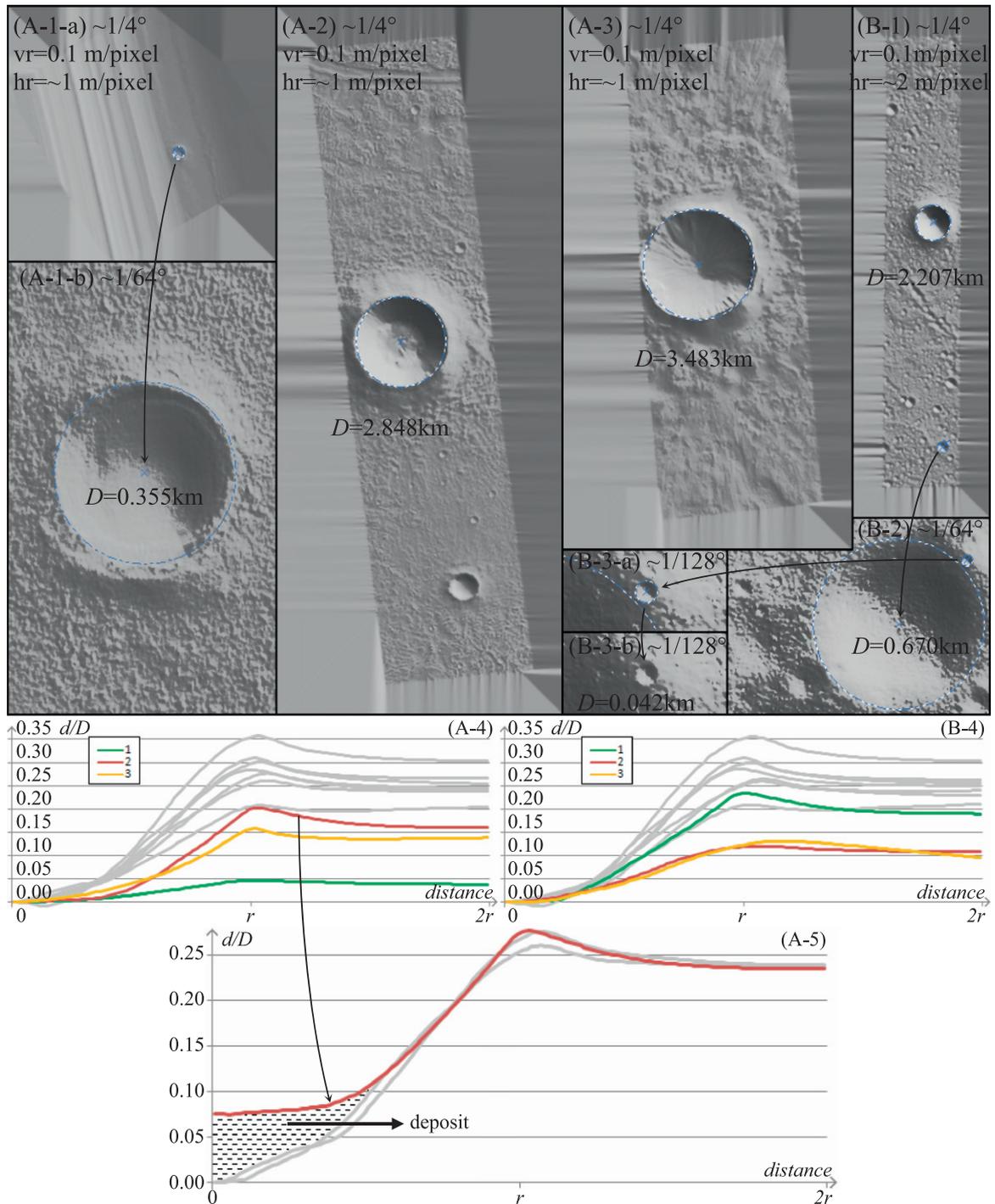
Target	Test							
	Mars CDA <sub>1</sub> -Canny (%)	Mars CDA <sub>2</sub> -Canny (%)	Mars CDA <sub>1</sub> -Shen-Castan (%)	Mars CDA <sub>2</sub> -Shen-Castan (%)	Moon CDA <sub>1</sub> -Canny (%)	Moon CDA <sub>2</sub> -Canny	Moon CDA <sub>1</sub> -Shen-Castan	Moon CDA <sub>2</sub> -Shen-Castan
cross	X	X	X	X	X	X	X	X
triangle	80.812	73.686	79.756	77.512	26.686	24.092	X	X
quadrangle	91.959	90.327	94.005	93.029	31.200	31.682	49.393	44.142
hexagon	96.879	96.897	95.613	95.310	96.733	96.349	85.760	85.694
math-crater-1	99.330	99.786	99.880	99.948	98.392	98.346	90.363	92.377
math-crater-2	100.000	100.000	100.000	100.000	99.869	99.890	98.625	98.552
math-crater-3	99.355	99.643	95.142	95.074	97.632	97.026	72.393	74.967
math-crater-4	100.000	100.000	100.000	100.000	99.872	99.873	99.259	99.329
lab-crater-1	98.924	99.634	98.962	99.065	96.403	96.482	87.092	89.862
lab-crater-2	99.657	99.933	98.808	99.517	99.374	99.559	98.105	98.432
lab-crater-3	99.440	99.725	98.957	99.269	99.225	99.286	97.281	96.909
lab-crater-4	97.854	98.492	99.212	99.455	97.752	97.786	95.006	96.549
lab-crater-5	98.817	99.126	97.502	97.888	98.780	98.779	61.641	60.429
lab-crater-6	98.980	99.602	98.884	99.357	98.558	98.821	91.907	93.095
lab-crater-7	97.381	97.491	98.434	98.793	96.833	96.766	88.719	87.231



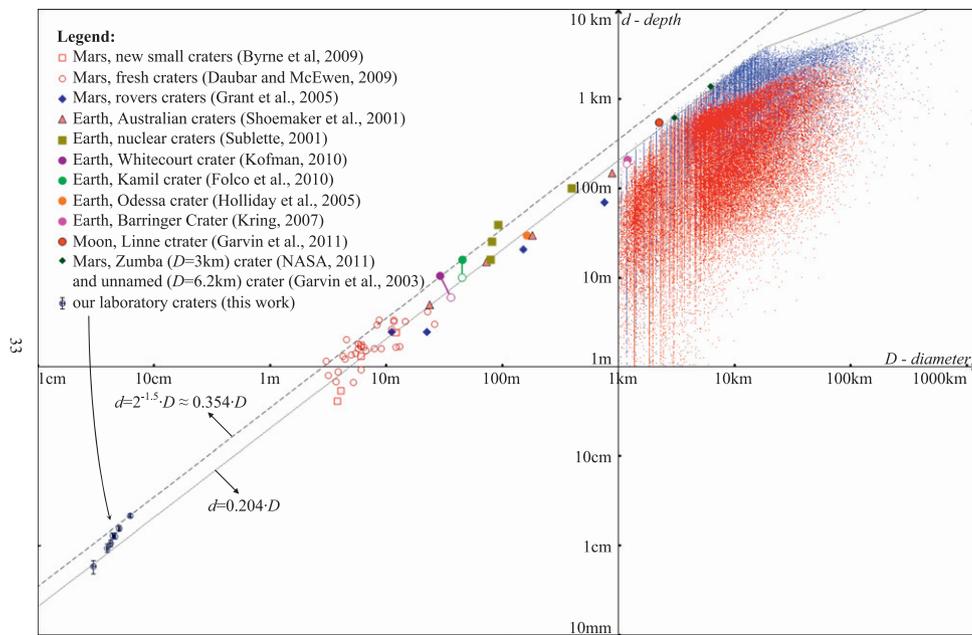
**Fig. 9.** Depth/diameter in log/log scale for Martian (A-1) and Lunar craters (B-1)—in each case five craters with some of the largest  $d/D$  ratios have been selected; comparison of profiles between laboratory and selected craters—these recent (with high  $d/D$  ratio) Martian (A-2) and Lunar (B-2) craters are similar to each other and to our laboratory craters; and the average profiles for four groups of craters (A-B-3) where, by contrast, there is a considerable difference between shallower Martian and deeper Lunar craters.

similar to craters, the hexagon is sufficiently similar, while the artificial objects triangle and quadrangle are somewhere between. The measure of similarity between artificial and real craters, based on the A-ROC evaluation and Eq. (1), can be used in the second approximation for more detailed analysis. The results for Martian and Lunar test-fields and all four variations of CDA are shown in Table 3. The observations are as follows: (1) the A-ROC curve is not identical for cases when the test-field is (CDA computations need to be performed only once per selected CDA) or is not emplaced in target topography, however differences are small and can be ignored; (2) the measure of similarity

between laboratory and real impact craters depends on the selected size of an emplaced laboratory crater, however this does not influence the results when all laboratory craters are scaled to the same size; (3) the 4th laboratory crater embedded in the Lunar test-field is not detected via CDA<sub>2</sub>-Shen-Castan when it is emplaced in the smallest size, therefore the conclusion is that for the Turing criteria it should be sufficient for passing the test that most detections are successful; (4) the overall measure of similarity is in some cases larger for mathematical models of craters than for laboratory or even real craters, we intentionally included this case in order to illustrate the potential overestimation



**Fig. 10.** Comparison of craters profiles from three Martian HiRISE (A-1, A-2, and A-3) and one Lunar LROC (B-1, B-2, and B-3) DEMs with profiles of laboratory craters (A-4, and B-4), and more detailed analysis in the case of Zumba crater—difference in profiles is most likely a deposit (A-5).



**Fig. 11.** Depth/diameter in log/log scale for all craters from LU60645GT catalog of Lunar craters (blue), MA132843GT catalog of Martian craters (red—superimposed over blue) and comparison with our laboratory craters and numerous other individual craters. (For interpretation of the references to color in this figure legend, the reader is referred to the web version of this article.)

problem; and (5) the resulting numbers are similar to each other and lead to similar conclusions whether we use Martian or Lunar test-field and which variation of CDA we use, this shows robustness and reliability of the overall approach.

### 3.7. Cross-comparison of profiles for standard and high horizontal resolutions

As noted in our previous work (Salamunićcar et al., 2012), there are some considerable differences between Martian and Lunar craters: (1) the transition of the depth/diameter ratio of the youngest craters on Mars occurs at  $D=5.8$  km, while on the Moon it occurs at  $D=18.4$  km, as shown in Fig. 9(A1 and B-1); (2) for Lunar craters the depth/diameter ratio and height of crater rim is approximately two times larger than for Martian craters, as shown in Fig. 9(A-B-3). However, the youngest (with highest depth/diameter ratio) Martian and Lunar craters do have, on the contrary, very similar profiles to each other and to the profiles of our laboratory craters, as shown in Figs. 9(A-2 and B-2). This confirms that our laboratory craters are good proxies for the scientific investigation of the youngest Martian and Lunar craters.

Using three Martian HiRISE and one Lunar LROC DEM, with much higher horizontal resolutions than available with global topography datasets, we additionally compared our laboratory craters with some craters that are much smaller than in the previous case, as shown in Fig. 10. One  $D=2.848$  km large Martian crater (A-2) and one  $D=2.207$  km large Lunar (B-1) crater have profiles with approximately the same depth/diameter ratio. In the case of the Zumba crater (A-2), the possibility of more detailed analysis is shown as well (A-5). When the profile is shifted in the graph upwards, it matches quite well the two profiles of laboratory craters for all distances between 0.5 and 2 radii. The difference is only for distances smaller than 0.5 radii. Our interpretation is that this difference is most likely a deposit, created after the formation of the transient crater. One possible application of the approach could be the impact melt volume estimates (Mazarico et al., 2011).

### 3.8. Depth/diameter ratio scaling

A depth/diameter in log/log scale for craters from recent Lunar and Martian catalogs and comparison with numerous other individual craters (Byrne et al., 2009; Daubar and McEwen, 2009; Folco et al., 2010; Garvin et al., 2003; Garvin et al., 2011; Grant et al., 2005; Holliday et al., 2005; Kofman, 2010; Kring 2007; NASA/JPL/University of Arizona, 2011; Shoemaker et al., 2001; Sublette, 2001) is shown in Fig. 11. Note how the largest depth/diameter ratio of the youngest craters is mostly independent of the crater's size and gravity despite many orders of magnitude of difference in crater depth or diameter. The transition between simple/small and complex/large craters is shown only at the top-right corner of Fig. 11. From this perspective as well, our laboratory craters are consistent with simple/small real impact craters on Mars, the Moon and Earth.

## 4. Conclusions

The result of this work is a complete framework for creation and evaluation of laboratory craters. The framework among others includes: (1) a new method for emplacement of laboratory craters in the topography of a planetary body; and (2) a new method for objective evaluation of laboratory craters which utilizes a CDA, the Turing test, and a new measure of similarity between laboratory and real craters. For the purpose of completeness, the framework also includes: (1) a procedure for creation of explosion-induced laboratory craters in stone powder surfaces using easily accessible silver acetylide ( $\text{Ag}_2\text{C}_2$ ) for explosive charges; (2) a method for 3D scanning of laboratory craters using a GOM-ATOS-I 3D scanner; and (3) a possibility of accompanying manual evaluation of laboratory craters using 2D topographical profiles extracted using our previously developed CDA. The approach has been verified using Martian and Lunar test-fields, in combination with artificial objects and simplified mathematical models of craters. In addition, several craters from high-resolution Martian and Lunar DEMs have been compared with our laboratory craters, showing that scientific investigation of real

impact craters using laboratory craters as proxies is possible for this case as well. Finally, the depth/diameter diagram in log/log scale of real impact craters on Mars, the Moon and Earth, with an extremely large range of depths and diameters, shows that our laboratory craters are consistent with real impact craters from this perspective as well. The major advantage of using the CDA for evaluation of laboratory craters, instead of, for example, a simple comparison of profiles, is that the CDA already has internal knowledge about craters' shapes, which can be utilized in order to achieve a higher quality of evaluation.

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